

# ECE 488 – Automatic Control

## Controllability and State Feedback Control

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Compulsory Course in Electronic and Communication  
Engineering  
Credits (3/0/3)

Course Webpage: <http://ECE488.cankaya.edu.tr>

## Reminder

### Previous Weeks

- Plant modeling
- Properties of transfer functions
- Stability and performance
- Feedback control
- Root locus method
- Nyquist criterion and bode plot
- Lead/lag compensator and PID-controller

### This week

- Controllability
- State feedback control

# Controllability: Preliminaries

## State-space Model

$$\begin{aligned}\dot{x}(t) &= Ax(t) + bu(t) \\ y(t) &= c^T x(t) + d_d u(t)\end{aligned}$$

## Transfer Function

$$G(s) = c_d^T (sI - A)^{-1} b + d$$

## Solution of the State Equation

$$x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)} bu(\tau) d\tau$$

## Example

Gap 1

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# Controllability: Definition

## Controllability Definition

*A linear system is called completely controllable if it is possible for each pair of states  $x_0, x_1$  to find a control input  $u(t)$  that moves the system state from  $x_0$  to  $x_1$  in a specified transfer time  $t_T$*

## Controllability Test by Kalman

*A linear system of order  $n$  is completely controllable if and only if the controllability matrix*

$$\mathcal{C} = [b \quad Ab \quad \dots \quad A^{n-2}b \quad A^{n-1}b]$$

*has full rank  $n$  ( $n$  is the order of the state space model)*

$\Rightarrow$  Check the rank of  $\mathcal{C}$  to verify controllability

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# Controllability: Example

## Computation

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# State Feedback Control: Alternative Controllability Test

## Hautus Test

*An eigenvalue  $\lambda$  of  $A$  is controllable (uncontrollable) if and only if the matrix  $\begin{bmatrix} (\lambda I - A) & b \end{bmatrix}$  has (does not have) full rank  $n$*

→ System is controllable if all eigenvalues are controllable

## Example

Gap 3

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# Stability: State Space Models

## Definition

*A linear system with the dynamic matrix  $A$  is asymptotically stable if all eigenvalues of  $A$  lie in the open left half plane*

⇒ Stronger condition than BIBO stability:  $G(s) = c^T(sI - A)^{-1}b + d$   
can be BIBO stable even if  $A$  has eigenvalues in the right half plane!

## Example

Gap 4

# Stability: Example

## Computation

Gap 5

# State Feedback Control: Idea

## Given

$$\begin{aligned}\dot{x}(t) &= A x(t) + b u(t) \\ y(t) &= c^T x(t) + d u(t)\end{aligned}$$

## Goal

- Use feedback of the state vector  $x$  to move the eigenvalues of the closed-loop system to desired locations

## State Feedback

$$u(t) = k^T x(t) + M r(t)$$

## Design Parameters

- Feedback vector  $k$ ; pre-filter  $M$

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# State Feedback Control: Block Diagram

## Illustration

Gap 6

## Practical Fact

- All state variables must be measurable

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# State Feedback Control: Closed Loop

## Computation

Gap 7

### State Space Model

$$\dot{x}(t) = \underbrace{(A + b k^T)}_{\tilde{A}} x(t) + \underbrace{b M}_{\tilde{b}} r(t)$$

$$y(t) = \underbrace{(c^T + d k^T)}_{\tilde{c}^T} x(t) + \underbrace{d M}_{\tilde{d}} r(t)$$

### Notation in Closed Loop

- Dynamic matrix  
 $\tilde{A} = A + b k^T$
- Transfer function  
 $\tilde{G}(s) = \tilde{c}^T (sI - \tilde{A})^{-1} \tilde{b} + \tilde{d}$

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# State Feedback Control: Closed Loop

## Closed-loop Requirements

- Stability  
 → All eigenvalues of  $\tilde{A}$  should lie in the OLHP
- Sufficient performance  
 → Suitable choice of the closed-loop eigenvalues (for example far away enough from the imaginary axis) using design parameter  $k$
- Zero steady-state error  
 → Suitable choice of the design parameter  $M$

## Questions

- When is it possible to assign the poles of the closed loop?
- How can we compute the design parameters  $k$  and  $M$ ?

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# State Feedback Control: Pole Assignment

## Choice of the Pole Locations

*If a linear system is completely controllable, then the eigenvalues of the closed-loop dynamic matrix  $\tilde{A} = A + b k^T$  can be assigned arbitrarily by a suitable choice of  $k$*

## Pole Assignment for Complete Controllability

- System order  $n$ : Choice of the closed loop characteristic polynomial (for example using desired eigenvalue locations)

$$p(s) = p_0 + p_1 s + \cdots + p_{n-1} s^{n-1} + s^n$$

→ We want that  $p(s) = \det(sI - A - b k^T)$

# State Feedback Control: Pole Assignment

## Pole Assignment for Complete Controllability

- Formula of Ackermann: Compute the vector  $v$  such that  $v^T = [0 \ 0 \ \cdots \ 0 \ 1] C^{-1}$

- Compute state feedback vector  $k$  using  $p(s)$  and  $v$

$$k^T = -p_0 v^T - p_1 v^T A - \cdots - p_{n-1} v^T A^{n-1} - p_n v^T A^n$$

## Example

Gap 8

# State Feedback Control: Example

## Computation

Gap 9

# State Feedback Control: Uncontrollable Eigenvalues

## Hautus Test

- Find uncontrollable eigenvalues
- All uncontrollable eigenvalues must also appear in the closed loop

## Pole Assignment by Comparison of Coefficients

- Determine the characteristic polynomial of the closed loop for  $k^T = [k_1 \ k_2 \ \cdots \ k_n]$  ( $k_1, \dots, k_n$  are free parameters)  
 $\rightarrow \det(sI - A - b k^T)$
- Choose a desired closed loop characteristic polynomial  $p(s)$  that preserves uncontrollable eigenvalues  
 $\rightarrow$  Evaluate  $\det(sI - A - b k^T) = p_0 + p_1 s + \cdots p_{n-1} s^{n-1} + p_n s^n$
- Compute the free parameters  $k_1, k_2, \dots, k_n$  by comparison of coefficients



# State Feedback Control: Example

## Computation

Gap 10

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# State Feedback Control: Example

## Computation

Gap 11

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# State Feedback Control: Pre-Filter

## Goal

- For unit reference step, we want to reach steady-state output value 1

## Solution

- Apply final value theorem to the closed-loop transfer function:

$$\begin{aligned}
 1 &= \lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} \tilde{G}(s) \\
 &= \lim_{s \rightarrow 0} ((c^T + d k^T)(sI - A - b k^T)^{-1} b M + d M) \\
 &= ((c^T + d k^T)(-A - b k^T)^{-1} b + d) M \\
 \Rightarrow M &= \frac{1}{(c^T + d k^T)(-A - b k^T)^{-1} b + d}
 \end{aligned}$$

→ Note: eigenvalues of  $-A - b k^T$  are non-zero

# State Feedback Control: Example

## Computation

Gap 12